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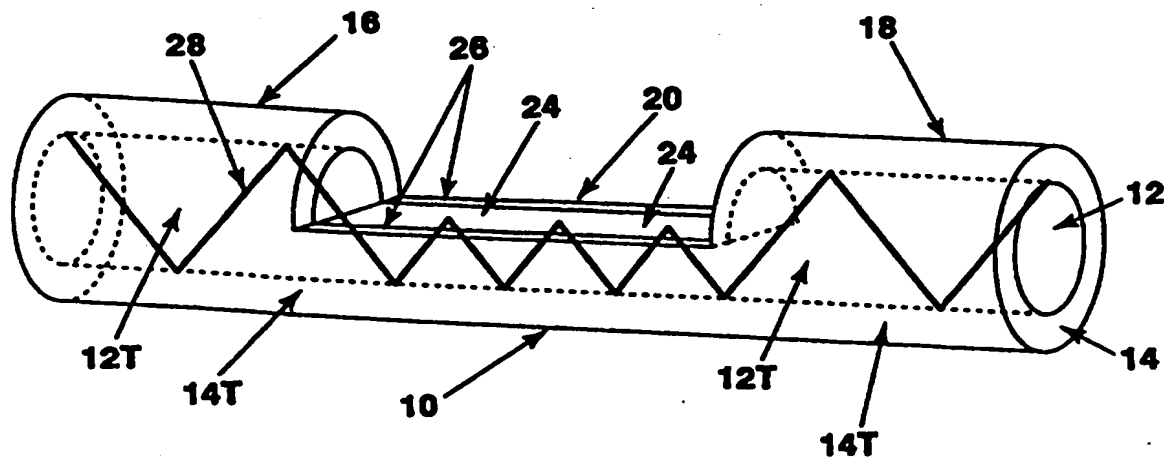
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(21) International Application Number: PCT/US95/10787 (22) International Filing Date: 25 August 1995 (25.08.95) (30) Priority Data: 08/315,288 29 September 1994 (29.09.94) US (71) Applicant: FOSTER-MILLER, INC. [US/US]; 350 Second Avenue, Waltham, MA 02254 (US). (72) Inventors: STEVENSON, William, A.; Four Wright Farm, Concord, MA 01742 (US). DRUY, Mark, A.; 38 Bonad Road, Arlington, MA 02174 (US). GLATKOWSKI, Paul, J.; Four Pinecrest Road, Littleton, MA 01460 (US). BOLDUC, Roy, A.; One Pine Street, Amesbury, MA 01913 (US). ZMORA, Hagai; 37 Hana Avrect Street, 76422 Rehovot (IL). (74) Agent: ERTMAN, Willis, M.; Fish & Richardson P.C., 225 Franklin Street, Boston, MA 02110-2804 (US).		(81) Designated States: CA, JP, MX, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE). Published <i>With international search report.</i> D2

(54) Title: **ATTENUATED TOTAL REFLECTANCE SENSING**



(57) Abstract

A radiation transmission optical fiber (10) for spectroscopic monitoring includes a transmission portion (16, 18) and a sensor portion (20); the transmission portion (16, 18) has a continuous core portion (12) and a continuous cladding (14) over the core portion (12); the sensor portion (20) has the cladding (14) removed from one side of the fiber and the core portion (12) exposed from the same side leaving the continuous cladding (14) intact over the opposite side of the core portion (12) of the sensor.

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ATTENUATED TOTAL REFLECTANCE SENSING**Background of the Invention**

5 This invention relates to spectroscopic technology and more particularly to technology for analyzing material using optical fiber-attenuated total reflectance technology.

 Spectroscopy is frequently employed in a
10 qualitative and quantitative analysis of materials. Infrared radiation detection techniques are frequently advantageous over spectroscopic techniques using radiation of shorter wavelengths, such as a visible or ultraviolet light, as organic and biological materials
15 have characteristic strong and relatively narrow unique identifying absorption peaks in the infrared region. Fourier transform infrared (FTIR) spectroscopic monitoring is useful in spectroscopy, as discussed, for example in Stevenson U.S. Patent No. Re.33,789, Bornstein
20 et al. U.S. Patent No. 5,070,243, Stevenson U.S. Patent No. 5,239,176 and Cook U.S. Patent No. 4,852,967. The material being analyzed or monitored may be gaseous, liquid or solid.

 This invention relates to the use of an optical
25 fiber as a multiple internal reflection (MIR) sensor and more particularly to the technology of using optical fibers as MIR sensors for performing both emission spectroscopy and absorption spectroscopic measurements of highly absorbing or highly scattering material, a
30 technique sometimes referred to as attenuated total reflectance (ATR) or evanescent wave spectroscopy.

Summary of the Invention

 In accordance with one aspect of the invention, there is provided a radiation transmission fiber for
35 spectroscopic monitoring that includes a transmission

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portion and a sensor portion. The transmission portion has a continuous core and continuous clad over one hundred percent of the transmission portion and between forty to sixty percent of the sensor portion. The remainder of the sensor portion has an exposed core surface (which is planar in particular embodiments but may be of other shape, such as cylindrical as appropriate), both the clad and core is either mechanically removed by grinding and polishing with suitable optical abrasive compounds or chemically removed by etching with a suitable etchant such as potassium hydroxide, zirconium oxychloride or hydrogen fluoride. The fiber may be as short as one centimeter and in a particular embodiment the sensor portion is about one centimeter long.

The sensor fiber core preferably is of a chalcogenide glass such as arsenic selenium tellurium, arsenic trisulfide, germanium selenium tellurium, arsenic germanium selenium; a heavy metal fluoride glass such as zirconium, barium, lanthanum, aluminum, sodium fluoride; fused silica or silicate glasses, or single crystal materials such as silver halides, thallium bromoiodide and cesium halide or sapphire. Preferably, the core has an initial diameter before ablation of at least fifteen micrometers but less than one millimeter and a refractive index greater than 1.5. Preferably, the fiber includes structure for changing the mode structure of the light beam propagating within the fiber such as a sharp bend(s) and/or by conical transition portions such as tapers.

In a particular embodiment, the transmission portion has a chalcogenide glass core of about 750 micrometers diameter and a cladding layer of chalcogenide glass of about 125 micrometers thickness; the sensor region core and cladding is ablated to approximately to the center of the core or to a total depth of about 500

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micrometers over a length of approximately one centimeter. The optical fiber in the transmission portion has a numerical aperture of 0.5, the glass core has a glass transition temperature of 136°C, a thermal expansion coefficient of $23.6 \times 10^{-6}/^{\circ}\text{C}$ and a refractive index at 10.6 micrometers wavelength of 2.81; while the glass cladding has a glass transition temperature of about 105°C and a refractive index of about 2.18 at 10.6 micrometers wavelength.

10 When such a sensor is encapsulated or potted in a typical optical epoxy, the cladding and/or core glass in the sensor region can be precisely ablated to the desired depth using conventional optical grinding and polishing techniques. The optical epoxy provides a firm, tough
15 support for the fiber and is ground and polished at the same rate as the glass. This provides a continuing firm support and mounting for the fiber that can be used for mounting and protecting the fragile sensor in a variety of different ATR probes. The evanescent wave propagating
20 at the polished surface of the core glass is not absorbed by the epoxy as the cladding glass on the underside of the sensor region is the only part that is in intimate optical contact with the epoxy.

By combining this asymmetrically exposed core
25 sensor with mode altering optical techniques such as simple bending in the shape of a U or using biconical tapers, qualitative and quantitative spectra measurements can be achieved that equal those obtained by the very best tapered core/clad sensors. One major difference is
30 the ease of reproducible manufacture. Fibers can be precisely bent using simple fixtures and can be permanently secured in a variety of suitable optical cements. Sensor ablation can be precisely controlled using a variety of well known optical grinding and
35 polishing equipment and techniques.

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Permanent protective support for the sensor may be provided by potting it in a hard, tough and durable optical cement that does not interfere with the operation of the sensor. This is particularly true when the sensor
5 is to be used for spectroscopically monitoring solids, abrasive powders, flowing viscous liquids, and high velocity gas streams.

In accordance with another aspect of the invention, there is provided a spectroscopy system that
10 includes a source of radiation for generating a broad band beam of radiation, a detector, a spectrum analyzing apparatus, and an elongated radiation transmission fiber for disposition in an absorption medium comprising a transmission portion and a sensor portion, and coupling
15 structure for optically coupling the transmission fiber to the source to transmit a beam of radiation through the fiber to the sensor portion and for coupling the absorbed beam back to the detector and the spectrum analyzing apparatus for analyzing the absorption medium in which
20 said sensor portion is disposed. The fiber length may range from less than one centimeter to ten meters or more. The transmission and sensor portions are described previously.

Brief Description of the Drawing

25 Other features and advantages of the invention will be seen as the following description of particular embodiments progresses, in conjunction with the drawings, in which:

Fig. 1 is a diagrammatic view of an evanescent
30 wave fiber optic sensor in accordance with the invention and Fig. 1A is a sectional view along the line 1A-1A of Fig. 1;

Fig. 2 is a diagrammatic view of another evanescent wave sensor in accordance with the invention;

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Fig. 3 is a diagrammatic view of an evanescent wave fiber optic sensor in accordance with the invention shaped in a U;

Fig. 4 is a diagrammatic view of still another evanescent wave fiber optic sensor shaped in a tight U bend with supplemental bends in the transmission portion just before and after the sensor region, and the entire fiber encapsulated in an optical cement;

Fig. 5 is a schematic diagram of a spectroscopic system employing the sensor of Fig. 4, Fig. 5A is an enlarged diagrammatic view, and Fig. 5B is a sectional view along the line 5B-5B of Fig. 5A;

Figs. 6 and 7 are schematic diagrams of variations of the system of Fig. 5; and

Fig. 8 is a graph of absorbance spectra of 100 percent isopropanol obtained with a spectroscopic system of the type shown in Fig. 5 and with a fiber optic sensor in accordance with the invention depicted in Fig. 4 and a tapered core/clad sensor of optimum design in accordance with Stevenson U.S. Patent No. 5,239,176.

Description of Particular Embodiments

With reference to the diagrammatic views of Figs. 1 and 1A, optical fiber 10 includes core portion 12 of arsenic, selenium, tellurium chalcogenide glass (AsSeTe) and cladding layer 14 of an arsenic sulfide (AsS) chalcogenide glass of lower refractive index. Fiber 10 has transmission portions 16, 18, transmission core portions 12T each having an outer diameter of approximately 750 micrometers and transmission clad portions 14T each having an outer diameter of approximately one millimeter. Sensor portion 20 has a length of about four centimeters with core portion 22 that is semicircular in shape and has relatively planar surface 24 that is approximately 750 micrometers wide, and semicircular cladding 26 that is approximately 125

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micrometers thick. As indicated, a light ray 28 propagates at reflection angles within the numerical aperture of the fiber. More reflections occur per unit length in the sensor region 20 due to the reduced cross section of the core portion 22 in the sensor region 20.

Fiber 10 is processed by encapsulating the entire fiber in a suitable optical cement and then grinding and polishing the sensor region 20 with suitable optical abrasives until the core portion 22 and attached cladding portion 26 are approximately fifty percent removed or ablated and smooth planar sensor surface 24 is exposed.

Fig. 2 depicts a fiber 10' which contains tapers between the transmission portions 16' and 18' and the exposed core surface 24' of sensor portion 20'. The tapers are in accordance with teachings of Stevenson U.S. Patent No. 5,239,176 and create more higher order modes in the sensor region 20' and then restore those modes to the normal propagating modes in the transmission region as shown by ray trace 28'; thus creating a more sensitive sensor.

Fig. 3 depicts another sensor fiber 10" in accordance with the invention in the shape of a squared U with bight portion 19 in which sensor region 20" is disposed. The sensor region 20" is approximately two centimeters long and includes planar core surface 24". Asymmetric reordering of the mode structure to higher order modes is accomplished in the ninety degree bends in the transmission portions 16", 18".

Fig. 4 depicts another sensor fiber suitable for mounting in small diameter - approximately five millimeters-"needle probes" designed for making evanescent wave spectral measurements in confined spaces such as test tubes or small diameter cylinders. A tight U bend 31 of approximately two millimeters radius is combined with relatively low angle bends 29 to produce

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higher order modes in the sensor region 40 in a compact sensor.

With reference to Fig. 4, sensor 30 includes an optical fiber of type similar to the fibers of the sensors shown in Figs. 1-3 and includes core portion 32 of about 750 micrometers outer diameter and cladding layer 34 of about 125 micrometers thickness. Fiber 31 is embedded in a suitable epoxy optical cement 36 such that terminal portions 38 at the end of transmission portions 31T are flush with the end surface 37 of epoxy 36. The fiber 30 is bent (29) twice, each at an angle of about 15° and again to form a tight U bend 31 of approximately two millimeters radius with the casing 36 having an outer diameter of about five millimeters. The epoxy casing support 36 is polished with suitable optical abrasives until the core portion 32 and attached cladding portion 34 are approximately fifty percent removed and a smooth planar sensor surface 40 is formed at an angle of about 15° to the axis of the cylindrical portion of casing 36. The tight U bend 31 of approximately two millimeters radius in the exposed surface 40, together with the relatively low angle bends 29 produce higher order modes in the sensor region 40 in a compact sensor that is about five millimeters in diameter and has a sensor surface 41 that is about one centimeter in length. A hard optically transparent coating of material such as magnesium fluoride may be applied to polished sensor surface 40 for use in contact measurement applications such as with abrasives, solids or human tissue.

Additional aspects of the sensor shown in Fig. 4 in combination with an FTIR analysis system are shown in Fig. 5. The sensor 30 is mounted in stainless steel probe support tube 42 in which coupling cables 44 are secured by suitable optical cement 45 and have coupling ends exposed within tube 42. Formed in tube 42 is keyway

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recess 46 and an annular recess that receives O-ring 48. Coupled to input transmission core clad fiber optic cable 44 is an FTIR spectrometer 50 of the Michelson interferometer type that includes infrared source 54, beam splitter 56 and focusing mirrors 58, 60. Coupled to core clad fiber optic output transmission cable 44 is an MCT (mercury cadmium teluride) detector 62, lock-in amplifier 64 and output processor 66 that includes display 68.

10 A sensor 30 of the type shown in Fig. 4 is inserted into housing 42 with axial and radial alignment by a key 47 that engages keyway 46 and the end surfaces 38 of the sensor fiber 31 are biased against the end surfaces of transmission cables 43, 44 by fluoroelastomer
15 O-ring 48. A removable protective sheath 70 may be disposed over the protruding portion of sensor 30, the slanted end surface 72 being flush with sensor surface 40 for applications for monitoring solid material such as abrasive particles or human tissue, and protruding
20 slightly where the material to be monitored is a liquid.

A sensor of the type in accordance with the invention depicted in Fig. 4 was connected to the analyzer apparatus depicted in Fig. 5. Measurements to determine sensor sensitivity, dynamic range, throughput
25 and signal-to-noise ratios were performed as follows. The system was set for resolution of four wavenumbers (4 cm^{-1}), one minute scan time (52 scans), and a spectral range of from 4000 cm^{-1} to 1000 cm^{-1} . Pure, anhydrous isopropanol was used as the test analyte.

30 With the sensor 30 connected, a single beam spectrum of the system in air was obtained. Then the sensor 30 was immersed in isopropanol and a second single beam spectrum of the system with the sensor 30 immersed in isopropanol was obtained. The second spectrum was

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ratioed against the first to produce an absorbance spectrum of isopropanol.

A tapered core/clad sensor of the type shown in U.S. Patent No. 5,239,176 with appropriate transmission cables was then substituted for the Fig. 4 sensor and cables according to the invention and similar spectra were obtained under the same experimental conditions.

Fig. 8 shows the comparative results. The ablated core sensor (Fig. 4) showed an absorbance peak height at 1126 cm^{-1} (a major analytical peak for isopropanol) of 0.55 absorbance units whereas the tapered sensor shows an absorbance value of 0.6 absorbance units for the same peak. RMS noise was measured for both spectra in the region between 1810 cm^{-1} and 1850 cm^{-1} . The total noise for the ablated core sensor of Fig. 4 was 0.00015 absorbance units resulting in a signal-to-noise ratio of 3,667 to 1. The total noise for the tapered sensor of the type shown in U.S. Patent no. 5,239,176 was 0.00024 absorbance units between 1810 cm^{-1} and 1850 cm^{-1} resulting in signal-to-noise ratio of 2500 to 1. In overall performance the sensors are approximately equivalent.

In another embodiment, shown in Fig. 7, the fiber includes a single transmission portion 16 with retro-reflector 92 at the remote end of sensor portion 20 so that the transmitted beam as modified by absorbance at sensor 20 is reflected back through portion 16 to beam splitter 94; and in another embodiment, shown in Fig. 6, the fiber 10 has a number of sensors 20 created according to the invention along its length.

While particular embodiments of the invention have been shown and described, other embodiments will be apparent to those skilled in the art, and therefore, it is not intended that the invention be limited to the disclosed embodiments, or to details thereof, and

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departures may be made therefrom within the spirit and scope of the invention.

What is claimed is:

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1. Radiation transmission fiber sensor apparatus for spectroscopic monitoring comprising an optical fiber (10) with a transmission portion (16, 18) and a sensor portion (20), said transmission and sensor portions (16, 18, 20) having a continuous core portion (12) and continuous cladding (14) over said core portion (12) throughout said transmission and sensor portions (16, 18, 20), characterized in that said cladding (14) in said sensor portion (20) is of asymmetric configuration such that an unclad core surface portion (24) in said sensor portion (20) is provided for exposure to material to be spectroscopically monitored.

2. Spectroscopy apparatus comprising a source (54) of radiation for generating a beam of radiation, spectrum analyzing apparatus (62, 66), a sensor including an elongated radiation transmission fiber (10) for disposition in a material of interest comprising a transmission portion (16, 18) and a sensor portion (20), said transmission and sensor portions (16, 18, 20) having a continuous core portion (12) and continuous cladding (14) over said core portion (12) throughout said transmission and sensor portions (16, 18, 20), and coupling structure (43, 44) for coupling said transmission fiber (10) to said source (54) to transmit a beam of infrared radiation through said fiber (10) to said sensor portion (20) and for coupling said fiber (10) to said analyzing apparatus (62, 66) for analyzing the absorption medium in which said sensor portion is disposed, characterized in that said cladding (14) in said sensor portion (20) is of asymmetric configuration such that an unclad core surface (24) portion in said sensor portion (20) is provided for exposure to material to be spectroscopically monitored.

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3. The apparatus of claim 2 wherein said source (54) is of the Michelson interferometer type and generates a beam of infrared radiation.

4. The apparatus of either claim 2 or 3 wherein said analyzing apparatus (62, 66) is of the Fourier transform type.

5. The apparatus of any preceding claim and further characterized by the provision of encapsulating support structure (36) surrounding said optical fiber (10) with said sensor surface (24) exposed at a surface of said support structure (36).

6. The apparatus of any preceding claim further characterized in that said cladding (14) in said transmission portion (16, 18) has a thickness sufficient to contain the evanescent field at wavelengths of analytical interest.

7. The apparatus of any preceding claim further characterized in that said core (12) is selected from the group comprising chalcogenide glass such as arsenic sulfide, arsenic germanium selenide, or germanium selenium telluride, heavy metal fluoride glass, oxide glass such as silica glass, and polycrystalline or single crystal materials such as thallium, bromoiodide, cesium halide or silver halide.

8. The apparatus of any preceding claim further characterized in that said sensor core portion (12) has a diameter in the range of 15 - 1,000 micrometers and a refractive index greater than 1.5.

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9. The apparatus of any preceding claim further characterized in that said transmission portion (16, 18) has a chalcogenide glass core (12) of about 750 micrometers diameter and a cladding layer (14) of 5 chalcogenide glass of about 100 micrometers thickness; and the exposed core surface (24) in said sensor region (20) has a length of at least about one centimeter and a width of less than one centimeter.

10. The apparatus of any preceding claim further 10 characterized in that said exposed surface (24) is planar and has a width of at least about one third the diameter of said core portion.

11. The apparatus of any preceding claim further characterized in that said fiber is formed in U-shape 15 with a bight portion (19) and said exposed core surface (24) extends into said bight portion (19).

12. The apparatus of any preceding claim further characterized in that said fiber further includes relatively low angle bends (29) in portions spaced from 20 said bight portion (19).

13. The system of claim 12 further characterized in that the angle of said low angle bends (29) is about 15°.

14. The apparatus of any preceding claim and 25 further characterized by the provision of sensor housing structure (42) and structure (47, 48) for releasably retaining said sensor in said housing structure (42).

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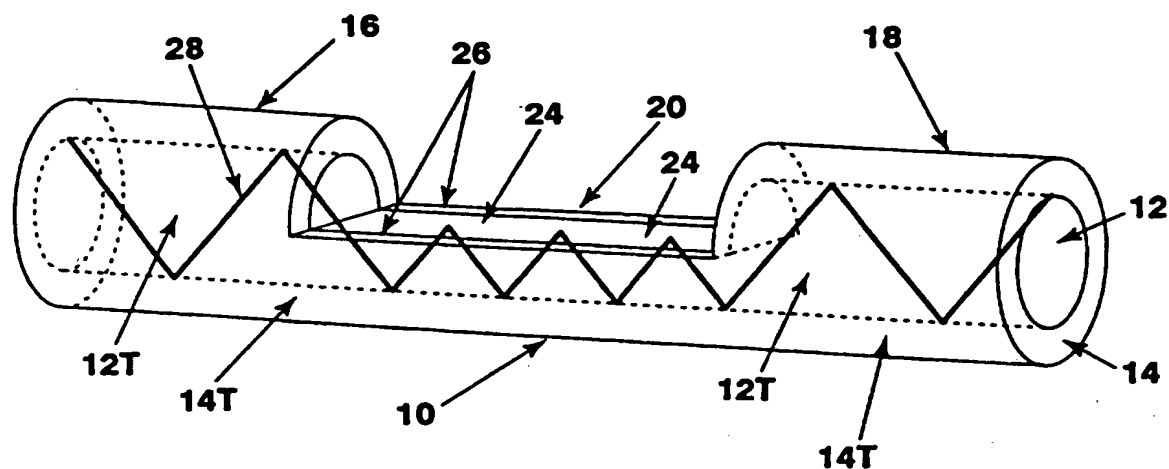


FIG. 1

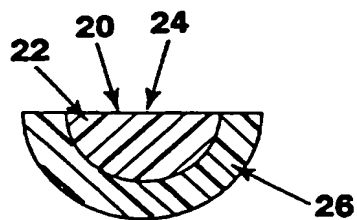


FIG. 1a

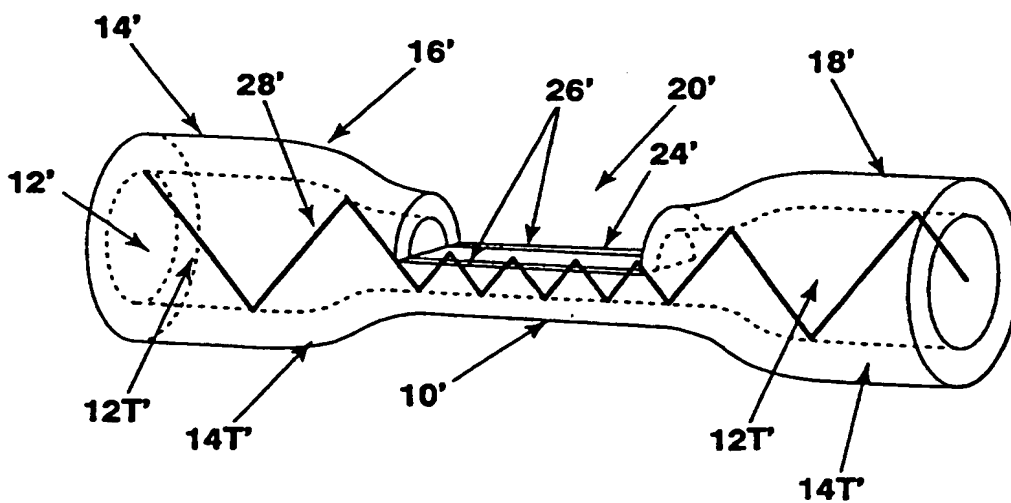


FIG. 2

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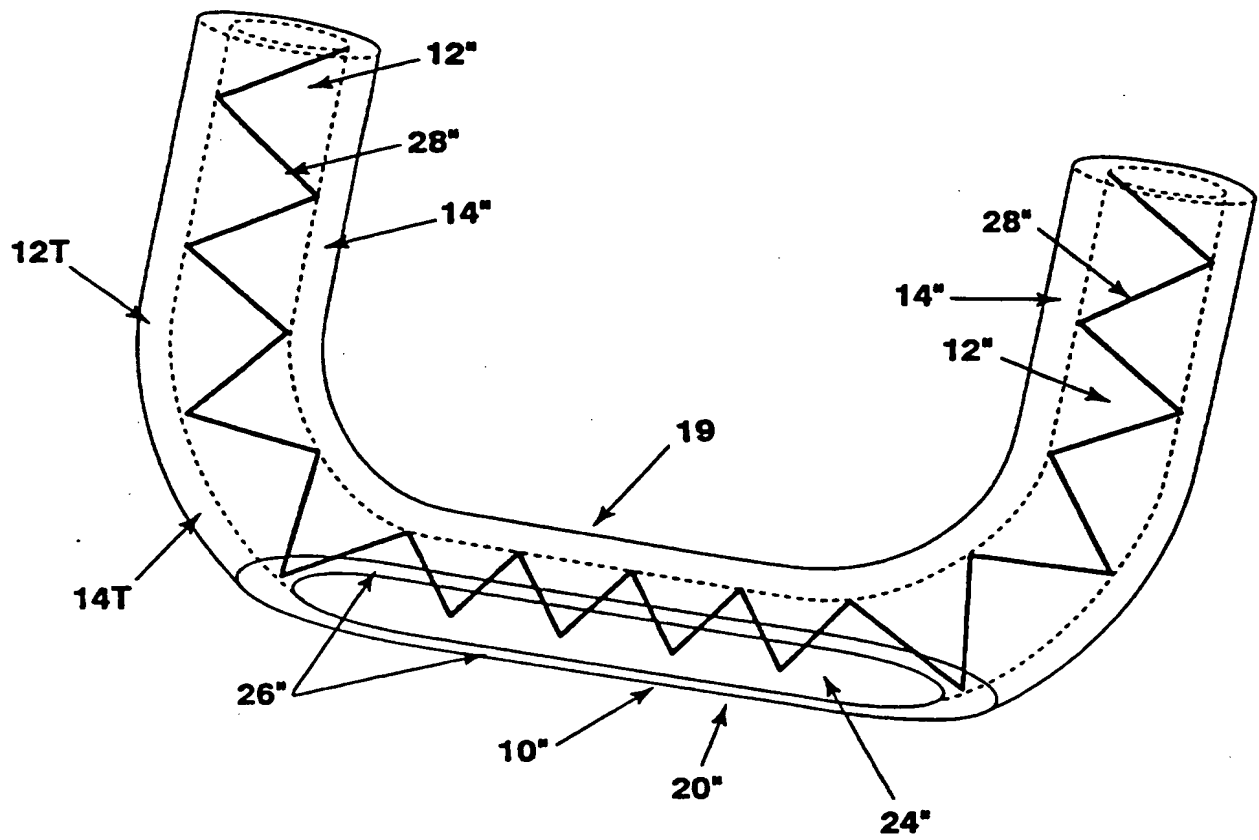


FIG. 3

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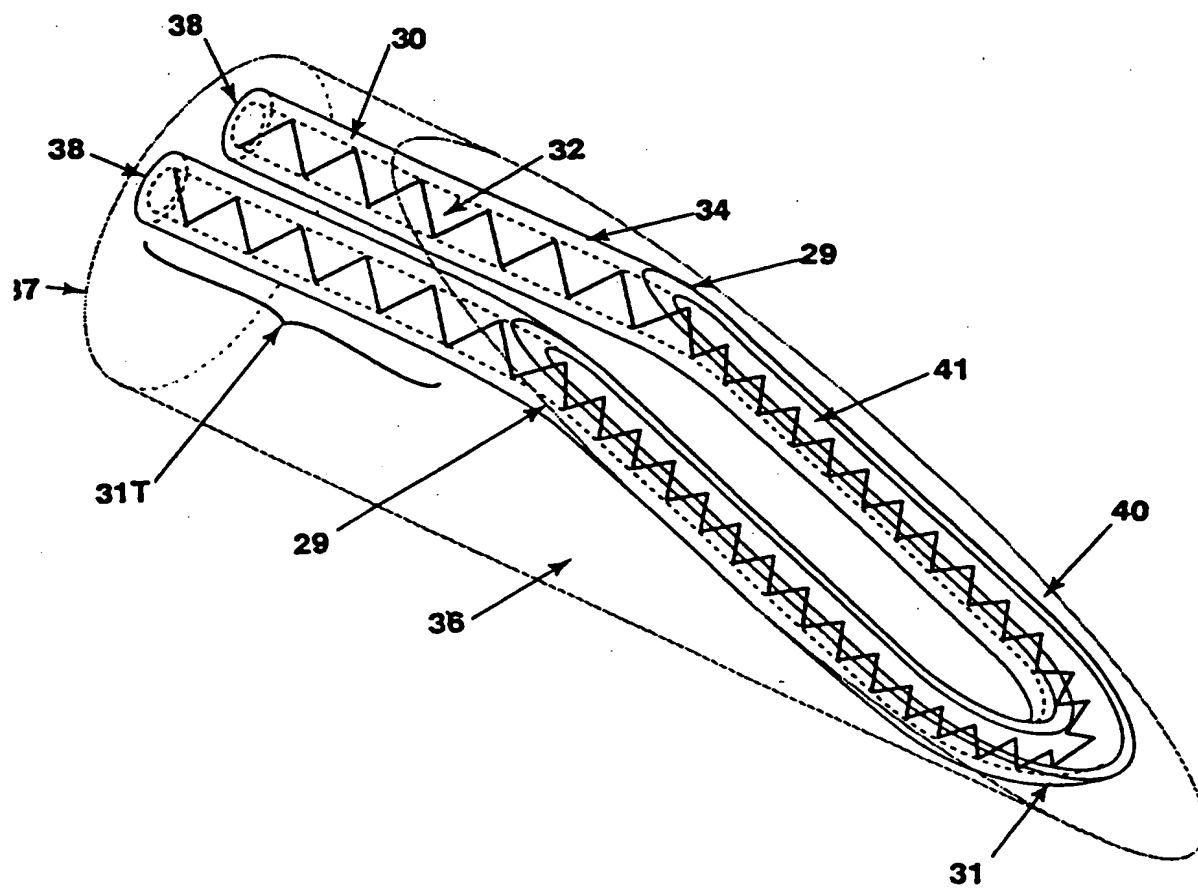


FIG. 4

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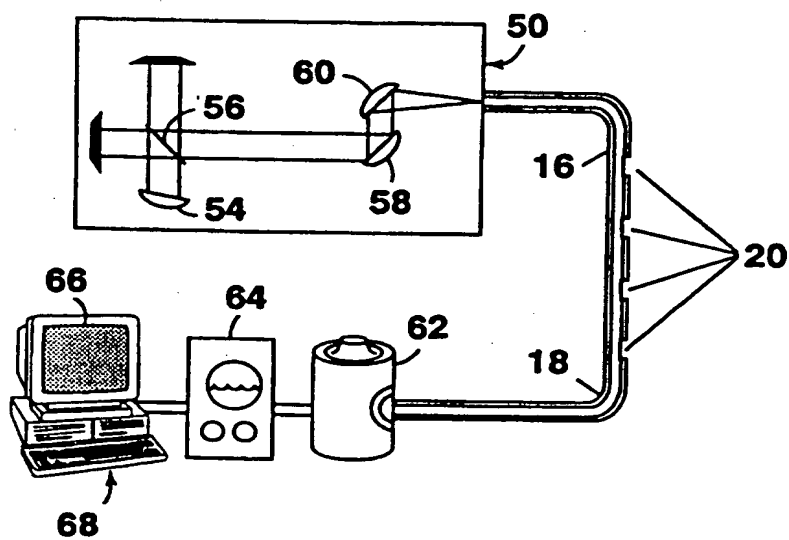
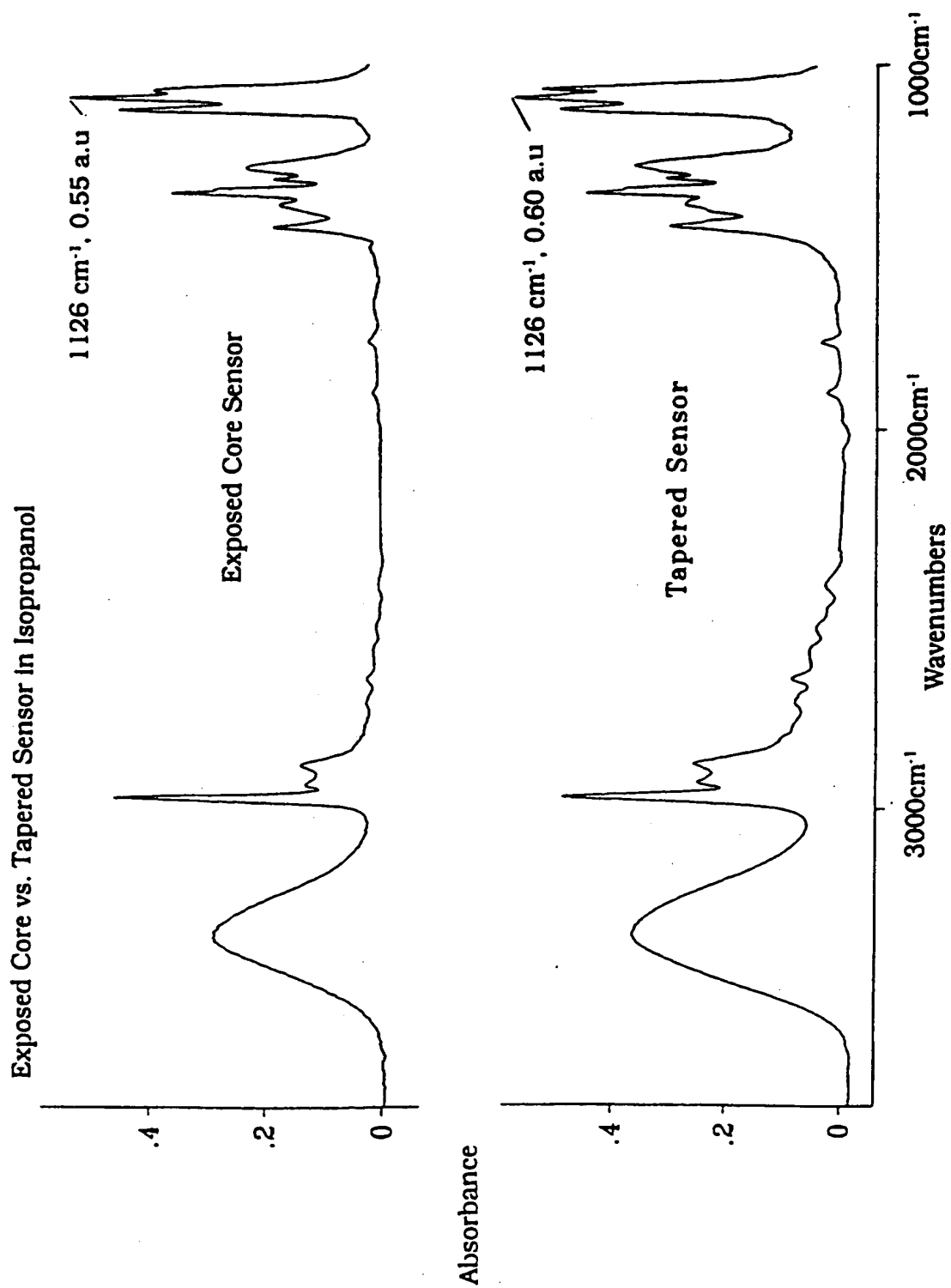


FIG. 6

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1 Minute Scan Time Res = 4 cm^{-1} **FIG. 8**

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US95/10787

A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) :G02B 6/02; G0IN 21/35

US CL :250/339.11,341.8;385/12,123

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 250/339.11,341.8;356/133;385/12,123

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched
CLASS 356 ATR DIGEST

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
NONE

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	DE 3,425,715 DROSSEL 16 JANUARY 1986 (16.01.86) SEE FIGURE 1-3	1
A,P	US A 5,436,454 BORNSTEIN ET AL. 25 JULY 1995 (25.07.95) SEE FIGURE 2	

☐ Further documents are listed in the continuation of Box C. ☐ See patent family annex.

* Special categories of cited documents:	T	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
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INTERNATIONAL SEARCH REPORT

International application No.
PCT/US95/10787

Box I Observations where certain claims were found unsearchable (Continuation of Item 1 of first sheet)

This international report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☐ Claims Nos.:
because they relate to subject matter not required to be searched by this Authority, namely:
2. ☐ Claims Nos.:
because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:
3. ☒ Claims Nos.: 5-14
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

Box II Observations where unity of invention is lacking (Continuation of Item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

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2. ☐ As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:
4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest.
☐ No protest accompanied the payment of additional search fees.

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